

# Controls on CO<sub>2</sub> Partial Pressure in Petroleum Reservoirs during Burial Diagenesis

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## Summary

Accurate prediction of  $CO_2$  partial pressure ( $pCO_2$ ) in petroleum reservoirs is important for reducing the risk in natural gas exploration (high  $CO_2$  abundance reduces the value of gas), improving reservoir quality prediction, assisting production and reservoir management operations and understanding of geological storage of  $CO_2$ . Previous models have provided significant insight into  $pCO_2$ -Temperaute relationships in sedimentary basins. However, most previous models neither considered a separate gas phase, nor the pressure effects on the minerals and aqueous species. In addition, the multi-component gas phase needs to be explicitly described and the effects of the presence of other gases on  $CO_2$  need to be quantified to accurately calculate the partial pressure. In this study, we developed a mineral-water-gas Interaction model to provide a comprehensive view of  $pCO_2$  as a function of temperature in petroleum reservoirs.

Our modeling results indicate that  $pCO_2$  values in petroleum reservoirs as a function of temperature are controlled not only by thermodynamic equilibrium between water and aluminosilicate and carbonate minerals, but also by the availability and composition of the coexisting initial gas. The model highlights that ignoring the presence of gas; pressure effects on the minerals, aqueous species and gases; or the presence of other gases may result in relatively large errors in calculated  $pCO_2$  values. Due to the irreversibility of aluminosilicate mineral reactions, carbonate- $CO_2$ -water equilibrium is one of the primary controls on pH and  $pCO_2$  in an uplift and re-subsidence scenario. The temperature versus  $pCO_2$  relationship calculated by the model for sedimentary basins with uplift and re-subsidence events deviates from the trend for sedimentary basins with monotonic subsidence.

#### Method

Calculations on geochemical equilibrium systems and  $pCO_2$  as a function of temperature in each system were aided with the computer codes PHREEQCI 3.4 (Parkhurst and Appello, 2013) with an improved thermodynamic dataset for minerals. CH<sub>4</sub> is considered representative of all hydrocarbon gases. Chemical equilibrium was assumed among  $CO_2$ , water, aluminosilicates, and carbonate minerals at T >50 °C. The gas phase was modeled at fixed total P (Parkhurst and Appelo, 2013), which was hydrostatic pressure at the study depth. The volume and mass of the gases are allowed to change. Water/rock ratio changes due to variations of the gas volume during the course of burial diagenesis were ignored. The gas fugacity coefficient and its solubility were calculated with the Peng-Robinson approach (Parkhurst and Appelo, 2013).

In this study, the base case refers to a gas-water-mineral system of 2 moles of total initial gas with a composition of 0%  $CO_2$  and 100%  $CH_4$  in contact with 1000 cm³ water and 4000 cm³ rock. P of the systems was calculated as hydrostatic pressure corresponding to depth. Reservoir T was calculated using an average geothermal gradient of 27.5 °C/km assuming a surface T of 15 °C. We slightly modified the average abundances of minerals from North Sea, Frio, Haltenbanken, and Wilcox for the starting

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mineralogy for our equilibrium model: quartz (76.5%), K-feldspar (8%), albite (4%), illite (0%), calcite (0.5%), kaolinite (9%), dolomite (1%), and siderite. For reservoirs with a complicated burial history, only forward reactions were considered and the backward reactions of some aluminosilicates were not allowed to proceed.

### **Results**

Temperature (and corresponding Pressure) vs.  $log(pCO_2)$  data from the literature for sedimentary basins with a relatively simple burial history (monotonic subsidence) are shown in Figure 1. Different models with different percentages of  $CO_2$  contents were constructed to model the observed  $log(pCO_2)$  in different fields: 5%  $CO_2$  for Patani, Thailand; 3% for North Sea, Norway; and 2% for Texas, USA. The Madison, USA; Alberta, Canada; and Paris Basin, France data are from aquifers and therefore do not have a gas phase.

Field data provided constraints on the starting gas composition and gas-water ratio (Fig. 2). It was observed that the mole fraction of  $CO_2$  increased with T (and P) without any external  $CO_2$  source. The models successfully reproduced the sharp increase of  $CO_2$  content around 140 to 190 °C and a slight decrease at 200 to 220 °C. Therefore,  $pCO_2$  values in petroleum reservoirs as a function of temperature are controlled not only by thermodynamic equilibrium between water and aluminosilicate and carbonate minerals, but also by the availability and composition of the coexisting initial gas. The model highlights that ignoring the presence of gas; pressure effects on the minerals, aqueous species and gases; or the presence of other gases may result in relatively large errors in calculated  $pCO_2$  values.

Due to the irreversibility of aluminosilicate mineral reactions (Helgeson, 1968; Helgeson et al., 1969), carbonate- $CO_2$ -water equilibrium is one of the primary controls on pH and  $pCO_2$  in an uplift and resubsidence scenario. The temperature versus  $pCO_2$  relationship calculated by the model for sedimentary basins with uplift and re-subsidence events deviates from the trend for sedimentary basins with monotonic subsidence (Fig. 3).

## **Conclusions**

In this study, we developed a mineral-water-gas interaction model to investigate the primary controls and provide a comprehensive understanding of  $pCO_2$  as a function of T in sedimentary basins. The model also addressed pitfalls in the calculations and limitations of previous models. Our model considered a gas phase, P effects on the minerals and aqueous species, and the effects of the presence of other gases (compositions of the gas phases) on  $CO_2$  on calculated  $pCO_2$  values. The model facilitates the investigation of the primary controlling factors of  $pCO_2$  in petroleum reservoirs. In addition, it addresses the pitfalls in the calculations and the limitations of previous models.

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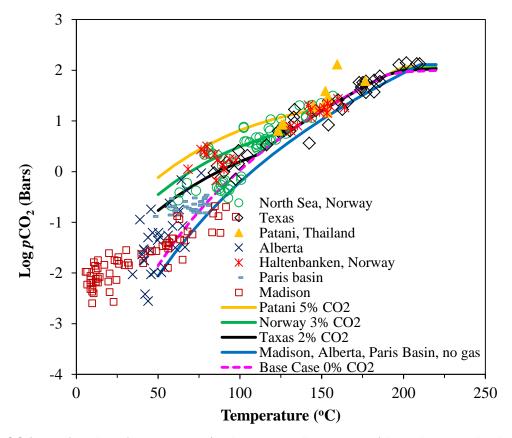


Figure 1. Log(*p*CO<sub>2</sub>) as a function of temperature (and corresponding pressure) in sedimentary basins with a simple burial history (monotonic subsidence). Symbols are field data and lines are simulation results. The purple dashed line shows the results from the base case (2 moles of total initial gas with a composition of 0% CO<sub>2</sub> and 100% CH<sub>4</sub>), while orange, green, and black lines represents cases with 5% CO<sub>2</sub> and 95% CH<sub>4</sub>, 3% CO<sub>2</sub> and 97% CH<sub>4</sub>, and 2% CO<sub>2</sub> and 98% CH<sub>4</sub>, respectively. The blue line represents saturation index of CO<sub>2</sub> defined as log(fugacity) of CO<sub>2</sub>. Madison, Alberta and Paris Basin are confined aquifers without gas phase (Coudrain-Ribstein et al., 1998) and therefore the values are log(fugacity of CO<sub>2</sub>) instead of log(*p*CO<sub>2</sub>). Data sources: Smith and Ehrenberg (1989) for North Sea and Haltenbanken, Norway; Franks and Forester (1984) and Smith and Ehrenberg (1989) for Texas, U.S.A.; Lundegard and Trevena, (1990) for Patani, Thailand; Connolly et al. (1990) for Alberta, Canada; Coudrain-Ribstein and Gouze (1993) for Paris Basin, France; Plummer et al. (1990) for Madison.

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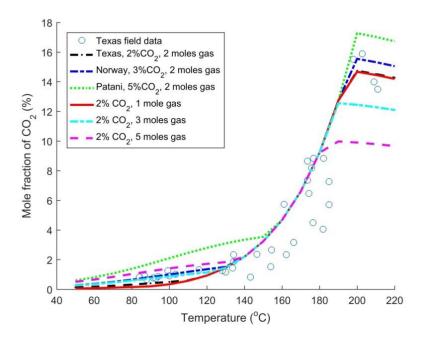


Figure 2. Mole fractions of CO<sub>2</sub> in the gas phase as a function of temperature (and corresponding pressure) for different starting gas compositions and total amounts of gas, compared with field data measured in Texas (Smith and Ehrenberg, 1989). Lines are simulation results.

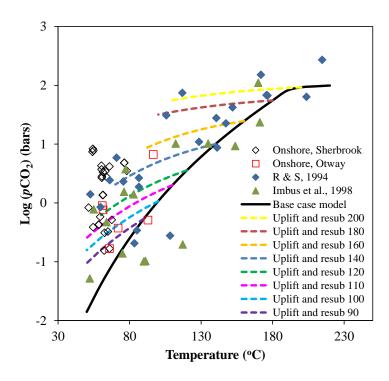


Figure 3. Log(*p*CO<sub>2</sub>) as a function of temperature (and corresponding pressure) in sedimentary basins with a complicated burial history (subsidence-uplift-resubsidence). Open symbols: Otway Basin, Australia; closed symbols: North Sumatra Basin. The solid line is the base case subsidence model. Dashed lines are a series of hypothetical pathways from different starting temperatures for the uplift-resubsidence events. Data sources: Watson et al. (2004), Reaves and Sulaeman (1994), and Imbus et al. (1998).

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